

# **Solving Vertical Pump Synchronous and Sub-synchronous Vibration Problems**

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Presented by:

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# Problems Analyzing Vertical Pumps

- **Lack of knowledge of foundation properties**
- **Effects of piping and motor attachment stiffness**
- **Lineshaft balance, alignment, and bearing eccentricities**
- **Typically, there are a large number of natural frequencies within the first fundamental harmonics of running speed**
- **Field testing is invaluable when trying to characterize a problem**

# Analysis and Solution Methods

- **Operational testing determines the natural excitation response of the pump**
  - **Steady operation is monitored to determine operating deflection shapes**
  - **Transient operation is monitored (particularly for variable speed machines) to determine problematic coincidences of excitation sources and natural frequencies**
- **Modal testing determines the natural frequencies of the structure and rotor**
- **Finite Element Analysis is calibrated to the installed field data and used to test practical fixes**

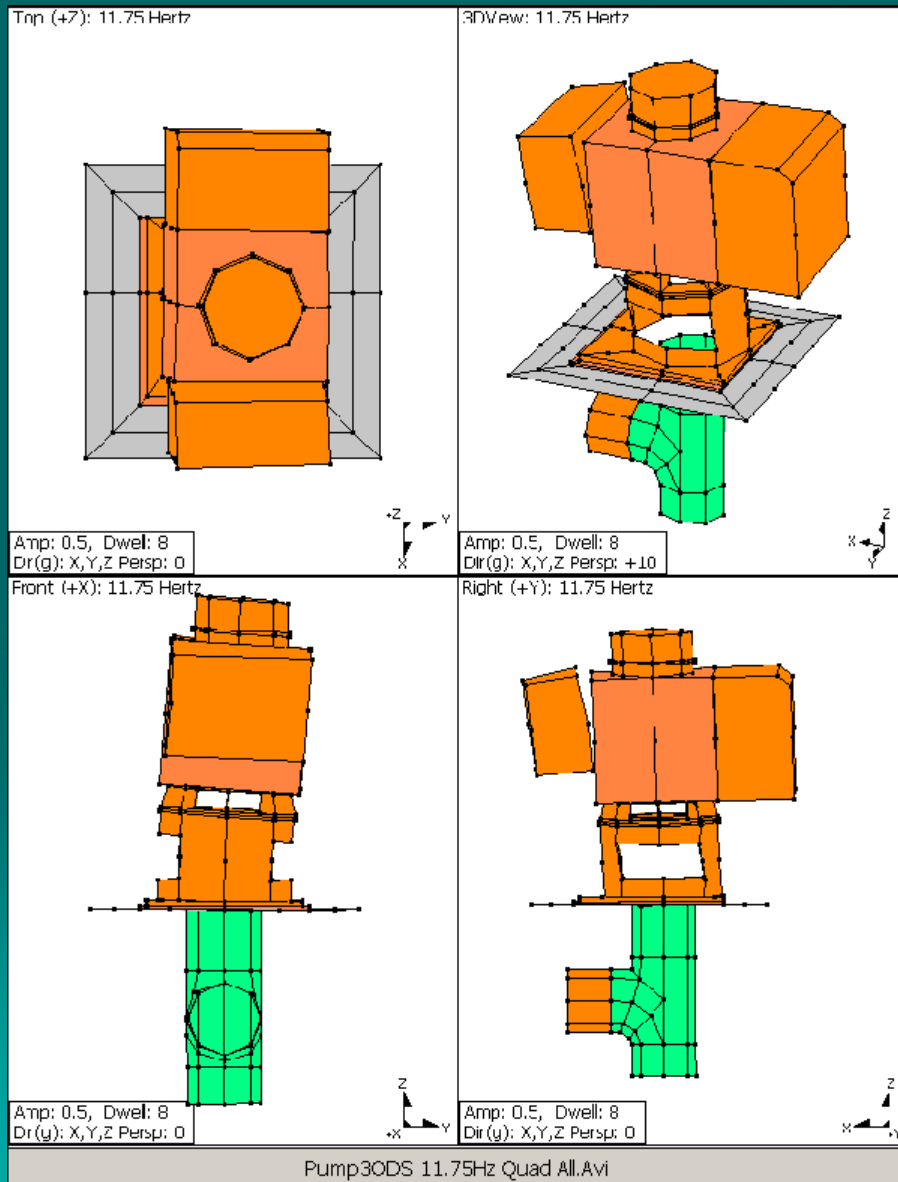
# CASE 1

## Synchronous Vibration due to Resonance with an Above Ground Mode

# Problem Statement

- **Large vertical turbine pumps (2000+ hp) in raw water service**
- **The maximum vibration at the top of the motor was 9 mils pk-pk which exceeded the specification by a factor of 3**
- **Pumps were not accepted by the owner, and the OEM had significant financial penalties for delay of pump commissioning**
- **Preliminary testing by the OEM resulted in suspicion of a structural resonance and / or excessive flexibility of the building structure**
- **Vibration amplitudes exceeded the specification even when the pumps were not operating**

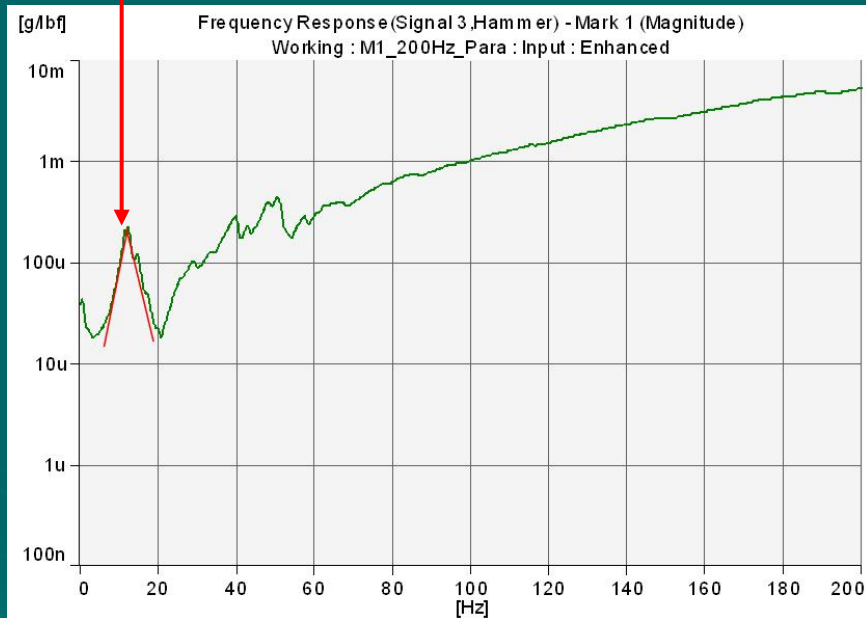
# Operating Deflected Shape Animation at Running Speed



**Pump #3 ODS at 11.75 Hz  
(705 CPM or 1X running  
speed)**

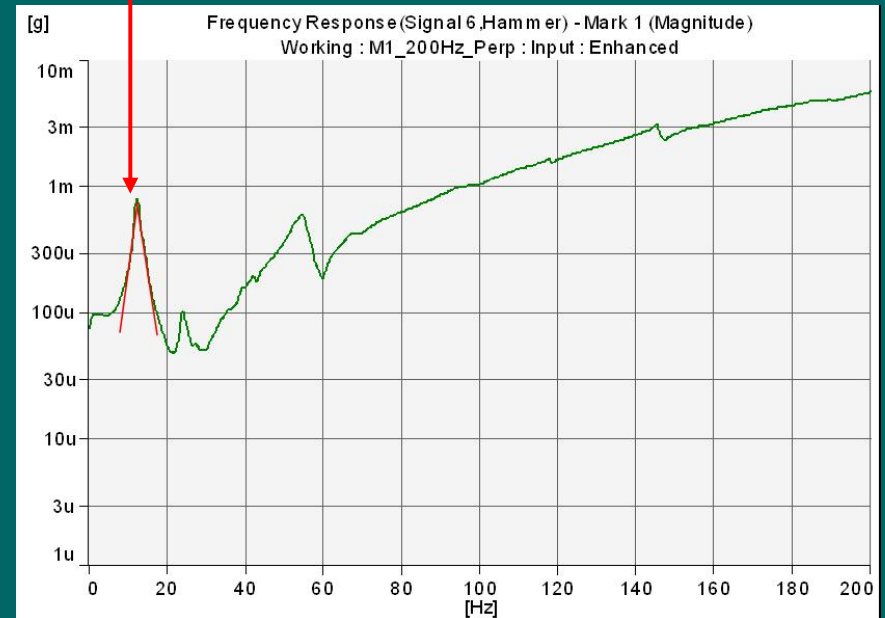
# Impact Modal Response at top of Motor

Running speed (11.75 Hz)



1<sup>st</sup> above-ground bending  
parallel to the discharge  
piping at 11.38Hz

Running speed (11.75 Hz)



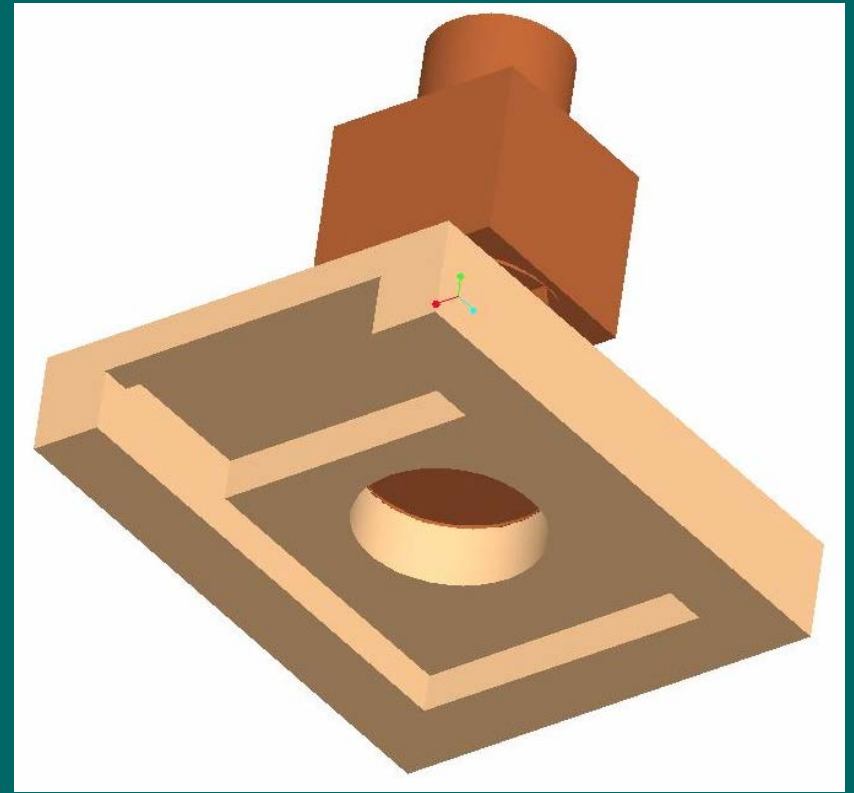
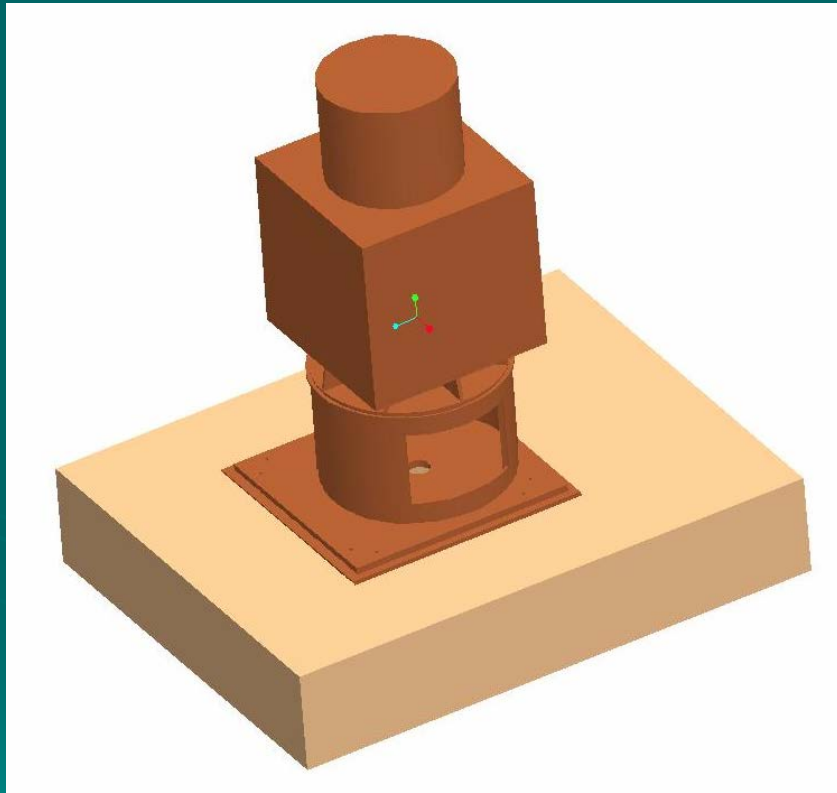
1<sup>st</sup> above-ground bending  
perpendicular to the  
discharge piping at 12.38Hz

# Preliminary Recommendations

- Increase the stiffness of the motor stand
- Improve motor rotor residual unbalance
- Improve the connection of the motor junction box
- Increase the building floor stiffness

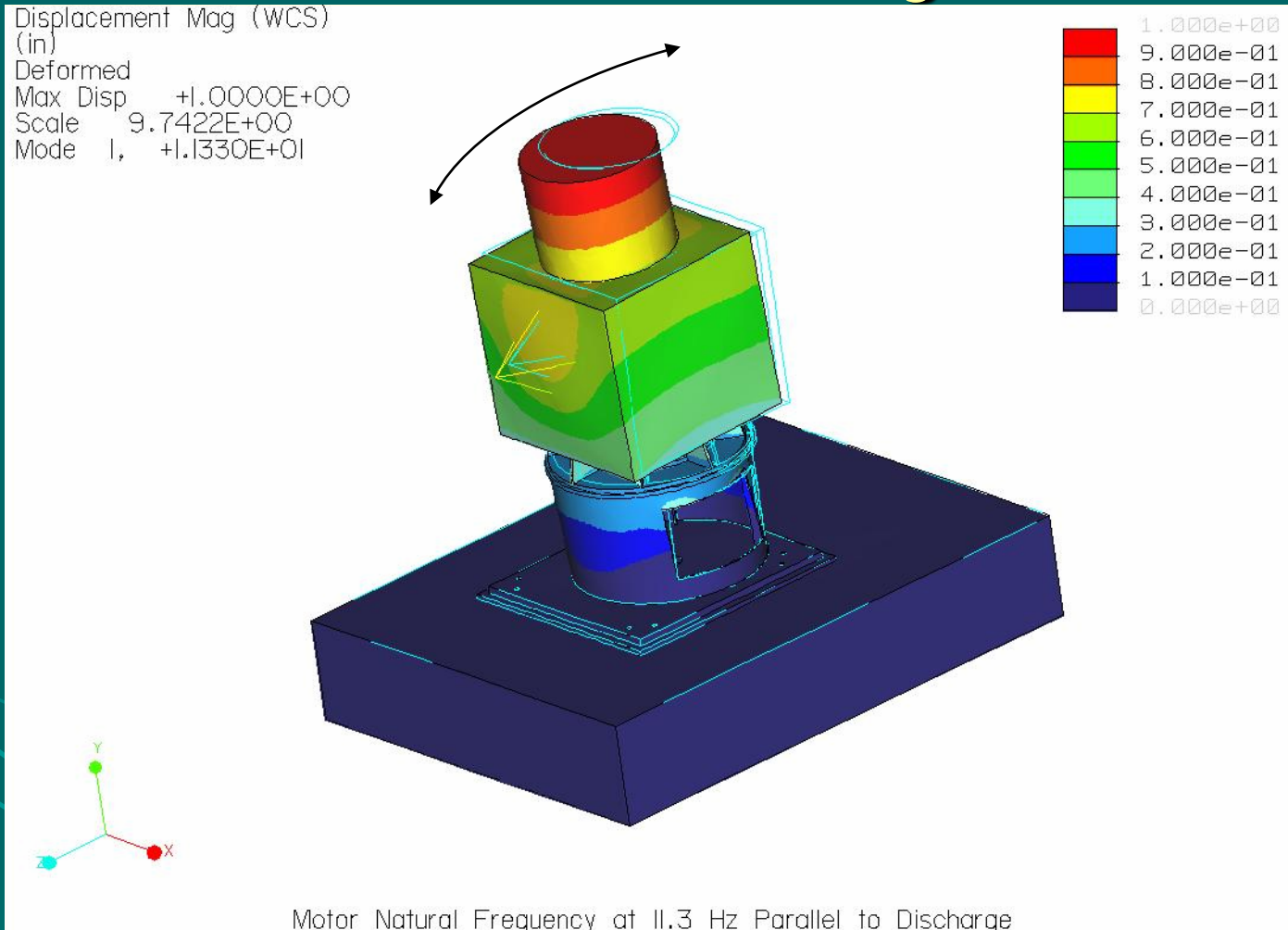


# FEA Modal Analysis



**Detailed solids model of the pump**  
Junction box not shown (mass element)

# FEA Modal Analysis

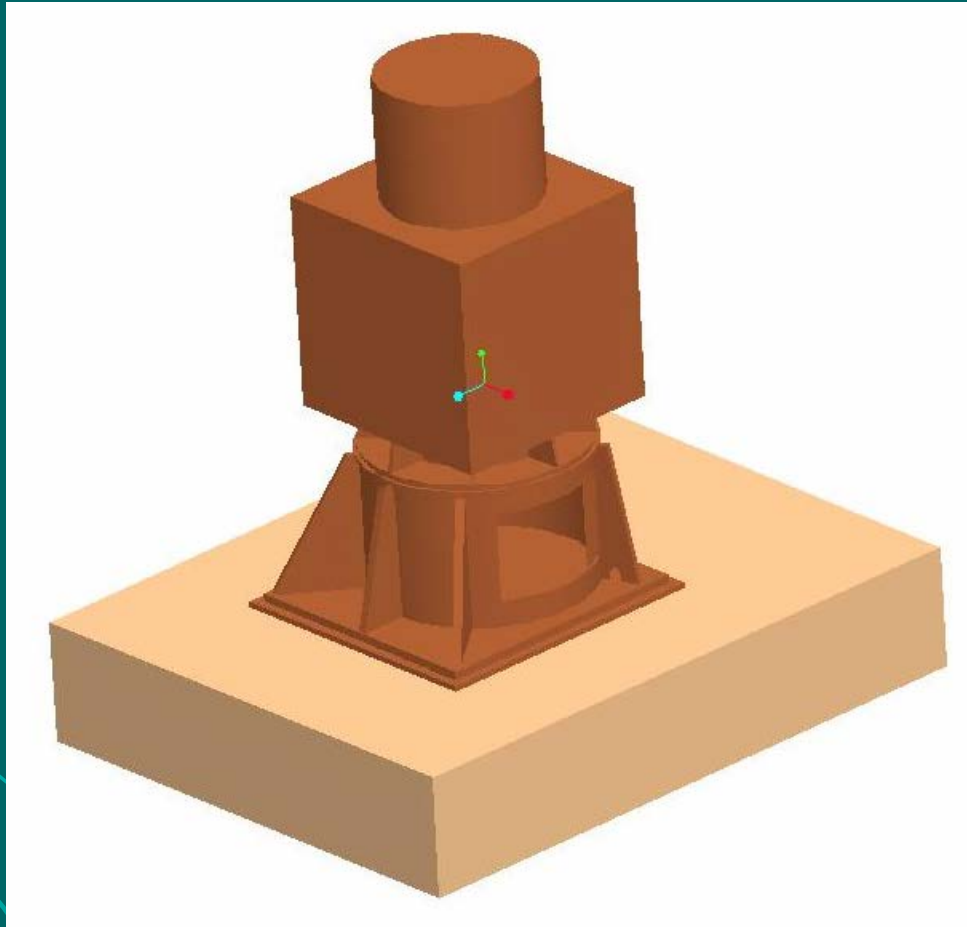


1<sup>st</sup> above-ground bending parallel to the discharge piping at 11.3 Hz

**Calibrated FEA model for original pump**

Junction box shown as mass element

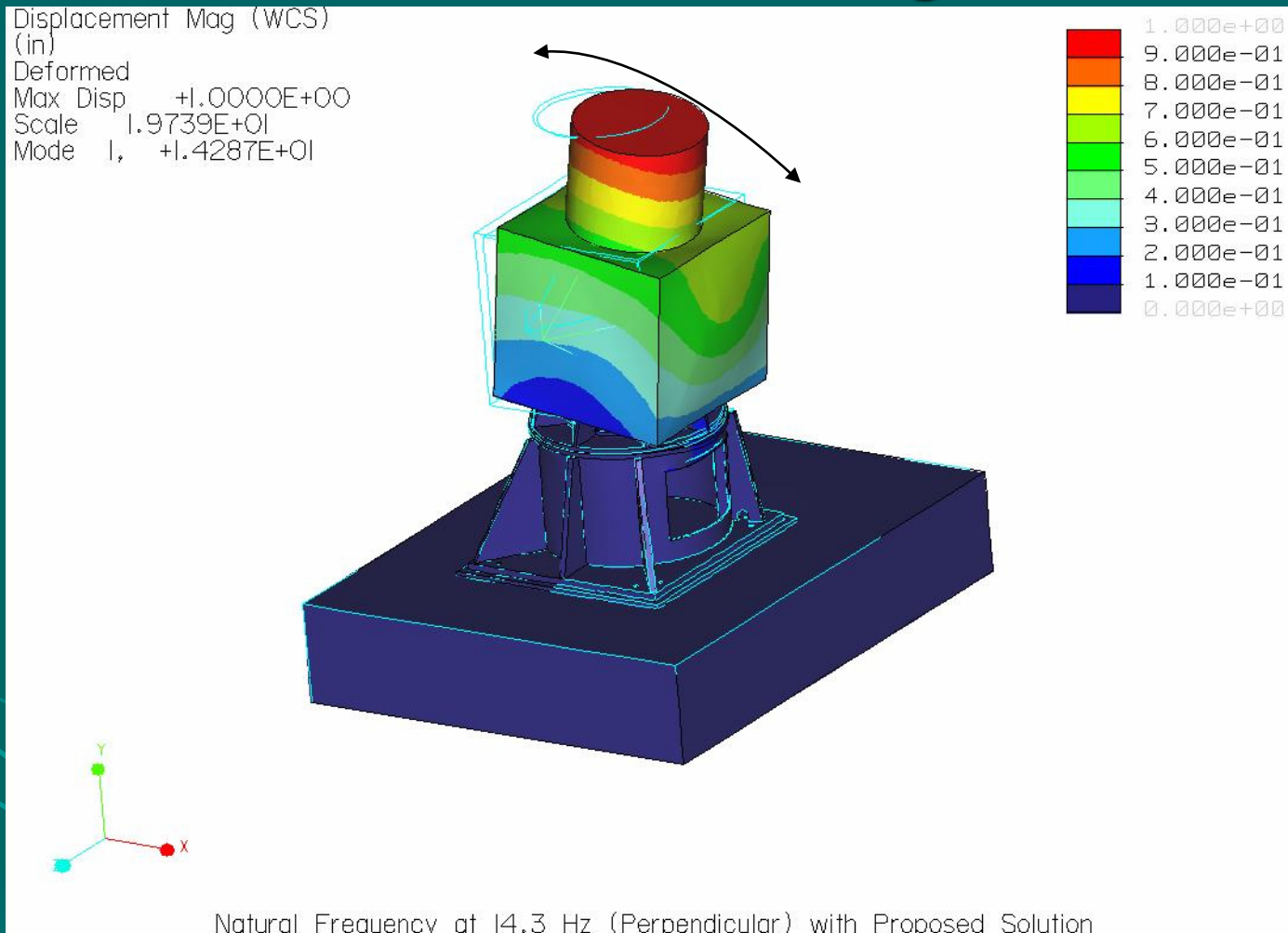
# FEA Modal Analysis



**Proposed modification of the motor stand**

Junction box not shown (mass element)

# FEA Modal Analysis



1<sup>st</sup> above-ground bending perpendicular to the  
discharge piping at 14.3 Hz

**Predicted structural natural frequency**

Junction box shown as mass element

# Summary

- **Vibration was being amplified by a structural natural frequency of the pump**
- **Modification of the motor stand resulted in the predicted shift in the structural natural frequencies and the desired 15% separation**
- **De-tuning of the structural natural frequencies resulted in a reduction of the vibration from 9.0 mils pk-pk to 3.0 mils pk-pk**
- **Vibration increased to 4.5 mils pk-pk due to unequal thermal expansion of the motor rotor**
- **Improving the motor residual imbalance resulted in a vibration amplitude of 1.5 mils pk-pk which did not increase with time**

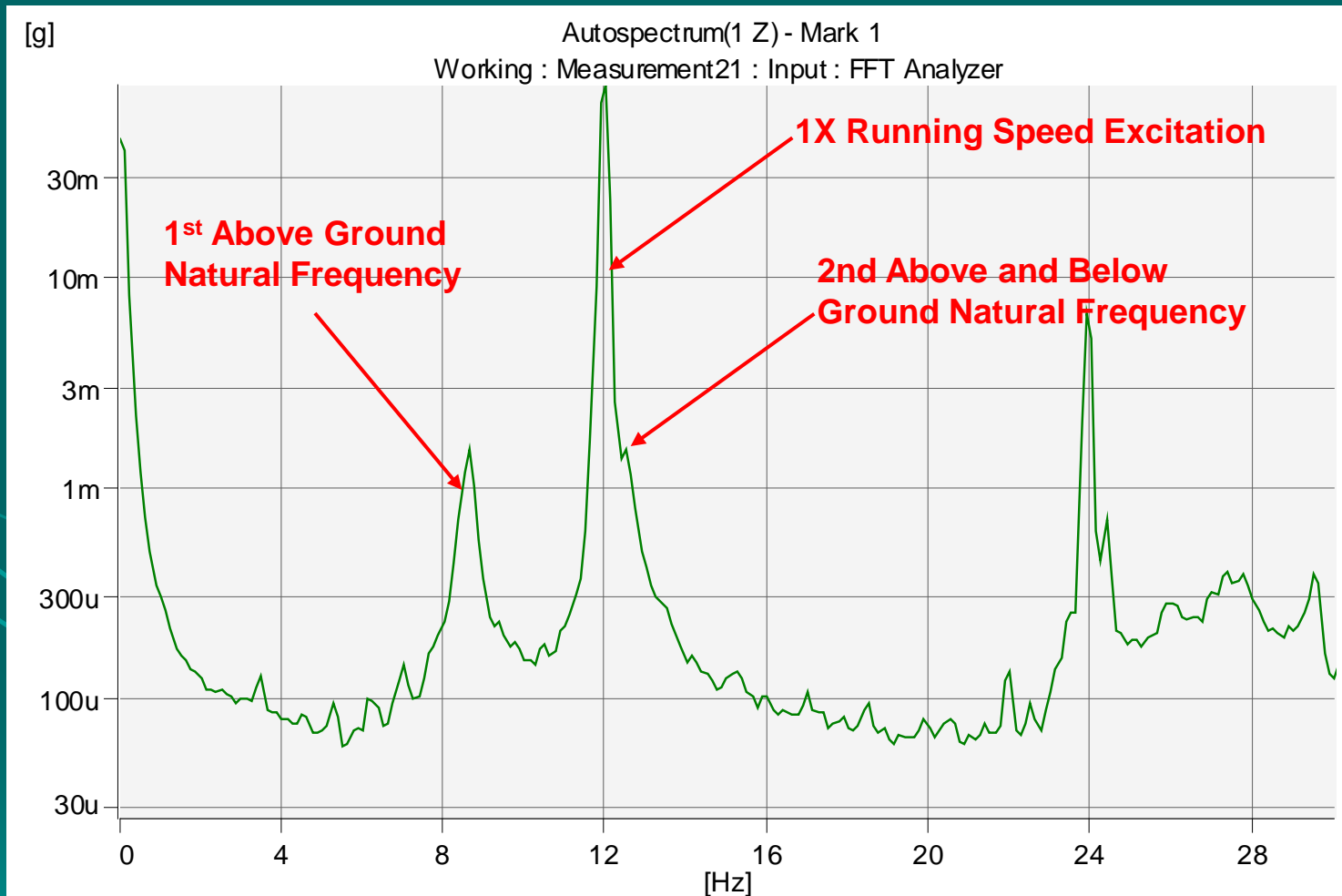
## CASE 2

# Excessive Synchronous Vibration due to Resonance with a Combined Above and Below Ground Mode

# Problem Statement

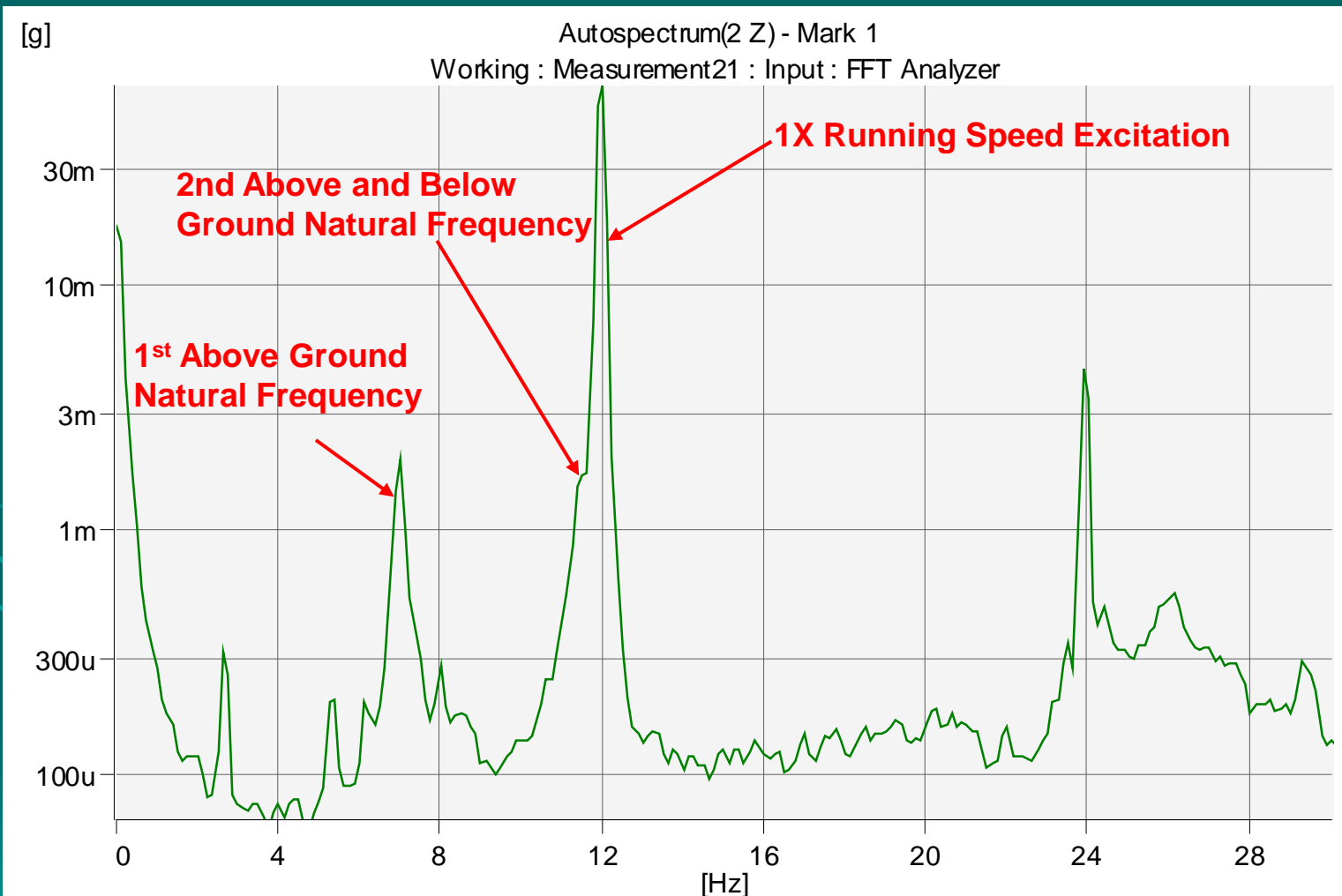
- **Circulating water pumps (1200 hp) installed at a new cogeneration plant in the Midwest**
- **Vibration levels measured on the motor were as high as 1.1 in/s RMS which exceeded specification and put commissioning of the plant in jeopardy**
- **Plant personnel had placed large steel plates on top of several of the motors which were successful in reducing vibrations on several of the pumps, but not on others**

# Typical Vibration Spectrum – Perpendicular to Discharge





# Typical Vibration Spectrum – Parallel to Discharge



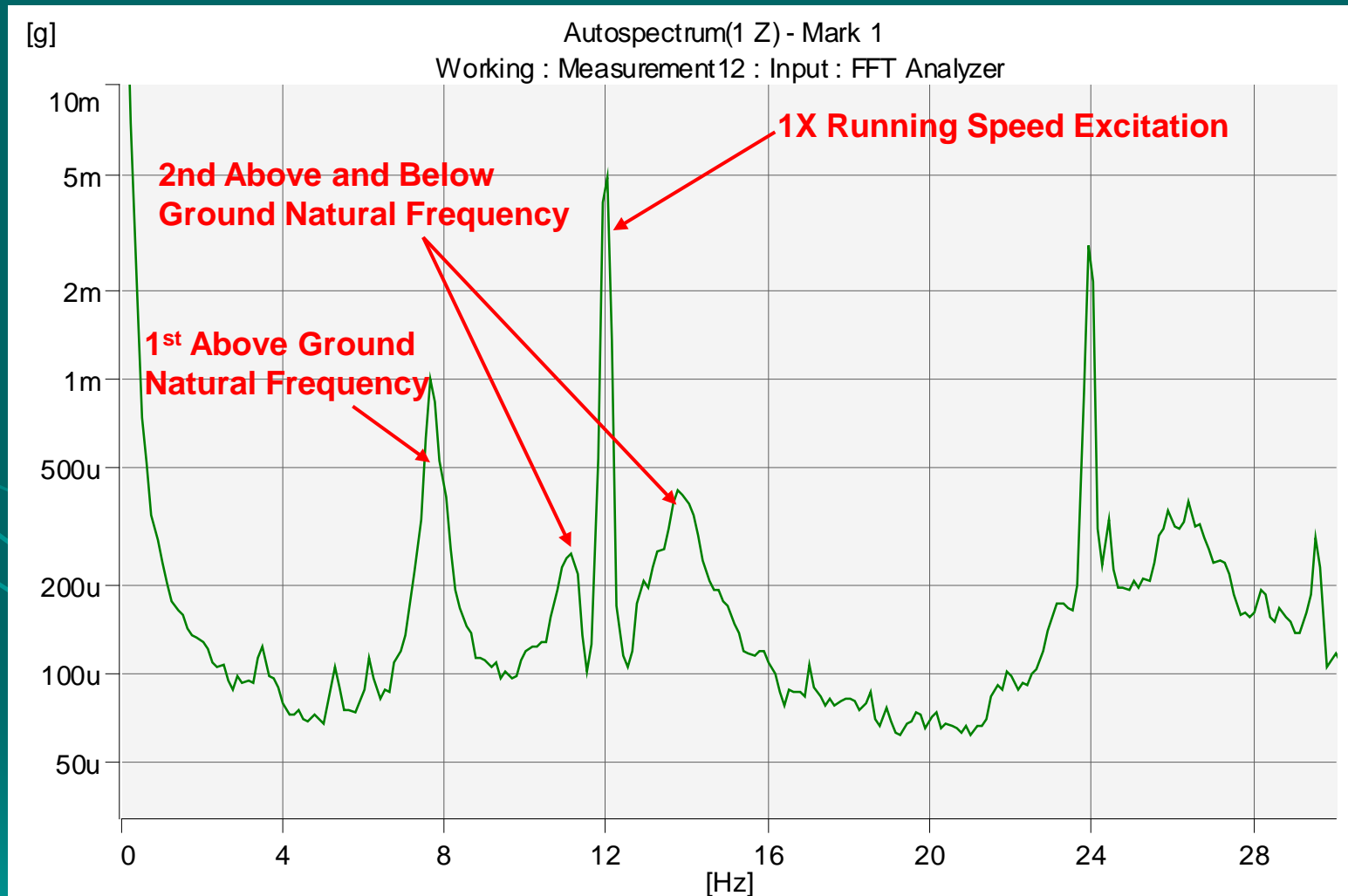
# Preliminary Conclusions

- **Vibration was being amplified by a structural natural frequency of the pump**
- **The problematic vibration mode had the top of the motor and the bottom of the pump moving in-phase with each other**
- **Due to differences in construction, the natural frequencies varied slightly from pump to pump**
- **Weights on top of the motor acted as “tuned-absorbers” for some pumps**
- **The flexibility of the conduit box similarly resulted in “tuned-absorber” effect**

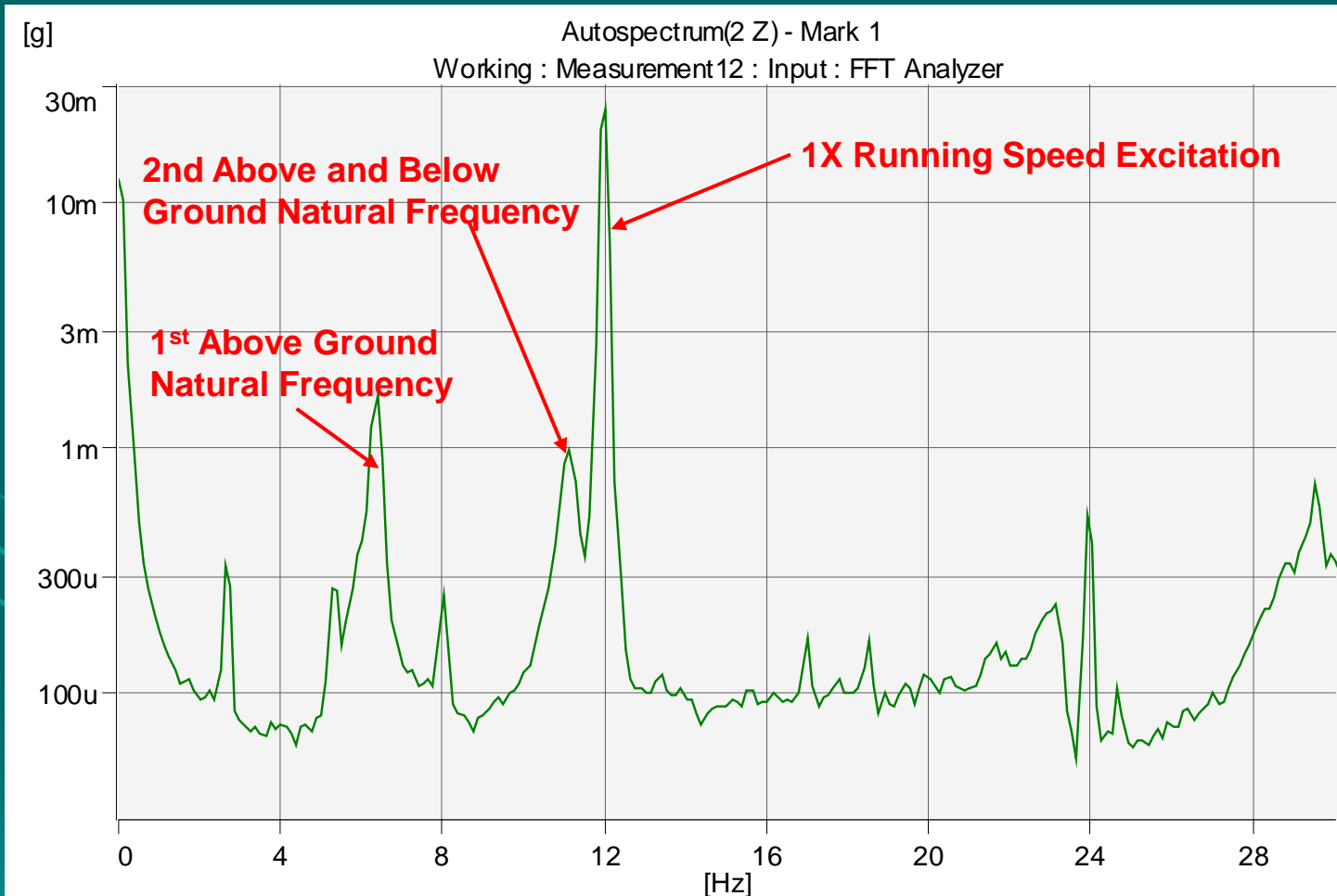
# Finite Element Analysis

- A finite element model was calibrated to match the test results
- Initial analysis predicted that more than 4,000 lbm of material needed to be added at the top of the motor to de-tune the natural frequency
- A more significant effect was predicted by adding mass to the bottom of the pump (suction bell)
- Recommendations varied from pump to pump, but all included added mass to both the suction bell and the top of the motor

# Vibration Spectrum - Perpendicular to Discharge with Added Weight



# Vibration Spectrum - Parallel to Discharge with Added Weight



# Summary

- **Vibration was being excited by a structural natural frequency which had combined above and below ground motion**
- **Adding mass only to the top of the motor would not have been sufficient to de-tune the below ground natural frequency**
- **With mass added to the top of the motor and to the suction bell, the vibration levels were reduced from 1.1 in/s RMS to below 0.28 in/s RMS and within the specification limits**
- **Stiffening of the junction box connection was recommended to reduce the chance of fatigue failure in the future**

# CASE 3

## Sub-synchronous Vibration due to Rotor and Bearing Rub

# Problem Statement



- Vertical turbine pumps in service offloading petroleum products from a tanker
- High synchronous and sub-synchronous ( $1/2X$ ) vibrations
- High temperatures were measured on the lineshaft bearings
- Product lubricated fiber reinforced Teflon bearings were used
- Concern over potential for heat or sparking in the bearings that could result in an explosion of the cargo



# Findings

- **Strong sub-synchronous vibration was measured with probes on column pipe and shafting at exactly  $\frac{1}{2}X$  running speed**
- **Inspection of the bearings discovered non-friable grit impregnating the relatively soft bearing material**
- **Investigation found that a new type of grit was used to clean the hull of the vessel**
  - **New grit was not sharp and friable**
  - **Residual grit in the hull after cleaning passed through the bearings**

# Conclusions

- **Exact  $\frac{1}{2}X$  running speed excitation is indicative of mechanical rubbing**
- **High bearing temperatures are also consistent with rubbing in the bearings**
- **Initial rubbing resulted in heat generation in bearings which expanded thermally**
  - **Coefficient of thermal expansion of Teflon is greater than that of surrounding steel, so the bearings reduced their clearance around the shaft and made the situation worse**

# Solution

- Short term solution was to change back to the original blast grit and to improve the procedure for cleaning residual grit
- The long term conservative solution selected by the tanker company was to change out the pumps and install submersible pumps which did not have lineshaft bearings
- Alternatives
  - Changing bearing material
  - Installing enclosing tubes to keep bearings isolated

# Conclusions

# Conclusions

- Synchronous vibration problems are typically due to poor balance and / or inadequate alignment
- After balance and alignment have been addressed in vertical turbine pumps, the excitation of the structural natural frequencies are the most common source of problems
- A combination of vibration testing and finite element analysis has proven to be valuable in diagnosing synchronous vibration problems and determining practical solutions
- Rubbing in bearings and seals typically results in a sub-synchronous vibration component at exactly  $\frac{1}{2}X$  running speed

# Conclusions

- **Rotordynamic instability can result in a sub-synchronous vibration component between 40% and 49% of running speed. Cases of rotordynamic instability have been experienced in vertical turbine pumps, but it is rare.**
- **Hydraulic problems such as suction recirculation can also result in sub-synchronous vibration**

# Recommendations

- **Testing combined with analysis are excellent tools when good engineering judgment and experience have not been successful in diagnosing and fixing vibration problems in vertical pumps**

**Thank you**

**Any Questions?**

