

# Evaluating and Correcting Subsynchronous Vibration In Vertical Pumps

## Case Study #8

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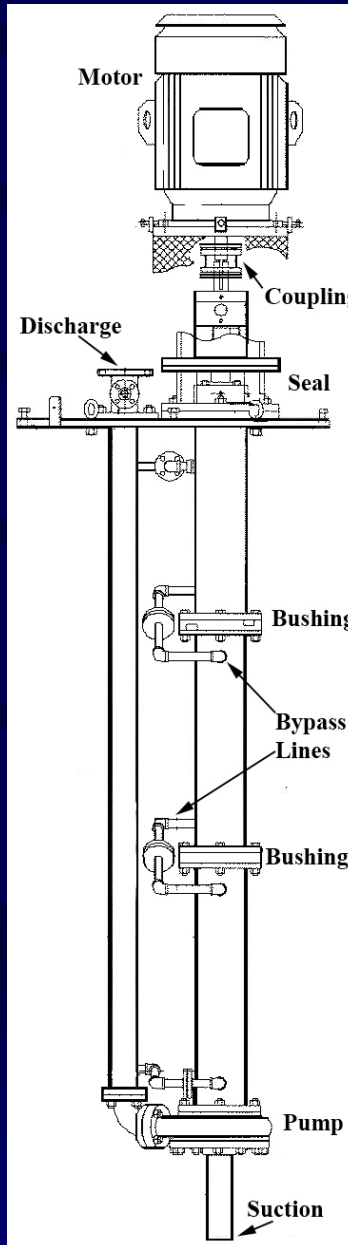
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# Case Study Overview

- New Vertical Pumps
- Liquid Sulfur Service
- Operating Speed – 3,575 RPM
- Primary Vibration Component at 1,750 CPM
- Shaft Whirling or Whipping Suspected
- Structural Resonance near  $\frac{1}{2} X$
- Solution

# Pump Layout



↑  
**164**  
**Inches**  
↓

# Pump System

6 Vertical Pumps in 3 Separate Sumps

Single Stage 81 GPM 219 Ft Head 40 HP

Molten Sulfur at 300 °F

Pump and Shaft are Steam Jacketed

4 Radial Bearings/Bushings

Top Bearing is also Thrust Bearing

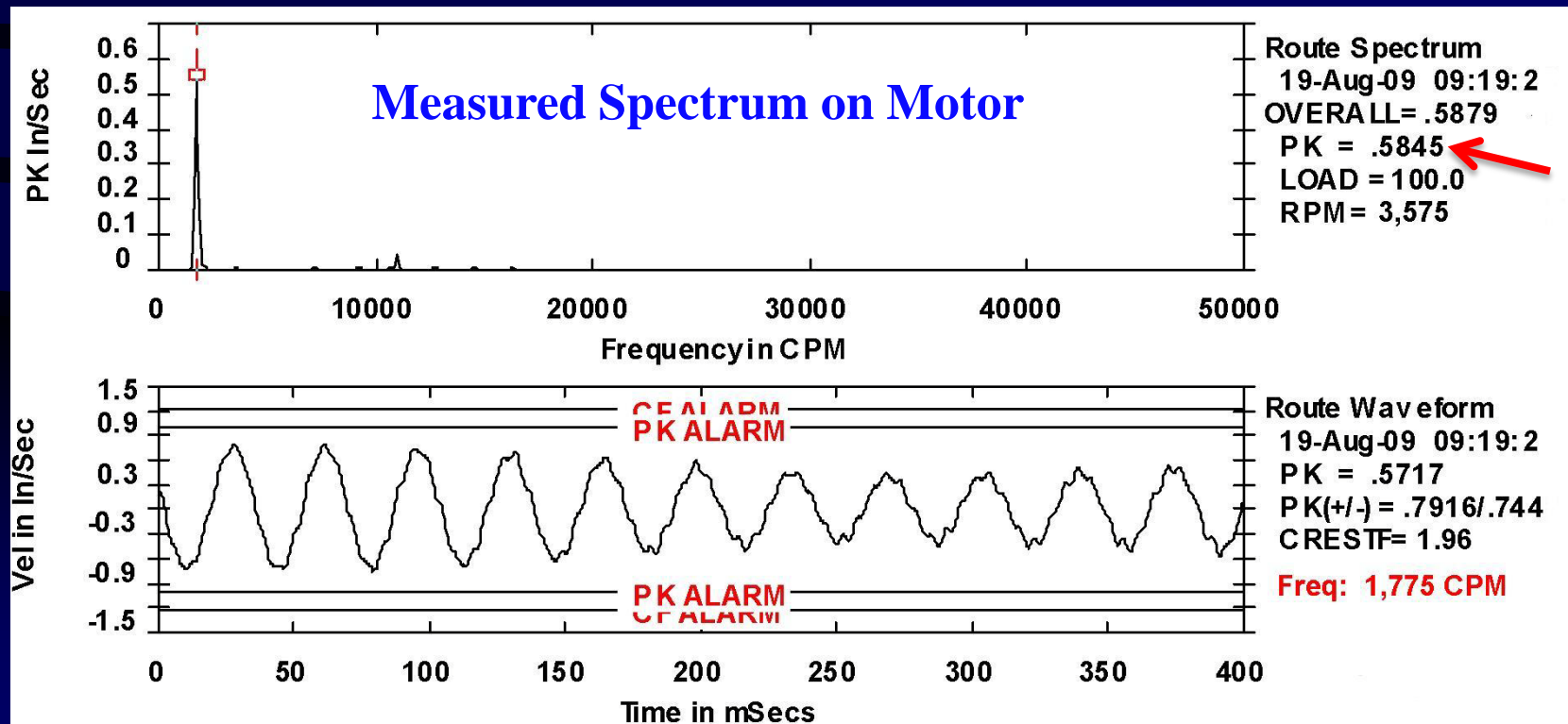
Line Shaft Bushings are Carbon Graphite

# History

- Hard “Sulcrete” Buildup in Sumps
- New Pump Mounting System Devised
- Initial Base Impact Test Showed Structural Natural Frequency in Excess of 5,000 CPM
- Initial Vibration Readings:
  - First Installation had 0.2 IPS at 1,710 CPM
  - Second Installation had 0.65 IPS at 1,750 CPM

# Vibration Measurements

- High Vibration on All Units
- Virtually no 1X (Running Speed) Vibration
- Most Vibration near  $\frac{1}{2}X$  Running Speed



# History

- Installed Impact Test Results on Motor

Bump Test Location	East - West Direction	North - South Direction
East Pump	<b>1,734 CPM</b>	<b>1,887 CPM</b>
West Pump	<b>1,657 CPM</b>	<b>1,887 CPM</b>

# History

- Clearly There was a System Natural Frequency near Half of Operating Speed
- What was the “Forcing Function”?
- Sulfur “whirl” Considered



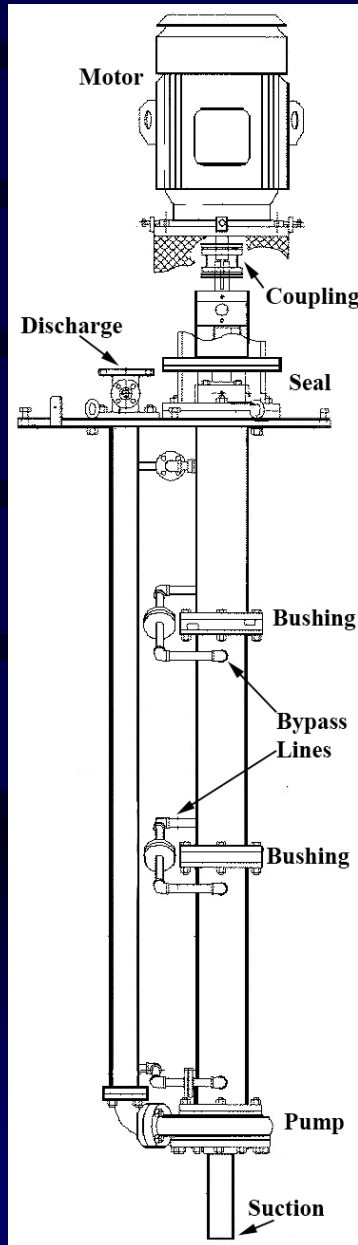
# Initial Attempts

- Reduced Weight of Coupling
  - No Significant Effect
- Possibly Stiffen Structure?
  - Probably would be Ineffective – Not Done
- Rotordynamics Analysis
  - Selected Approach

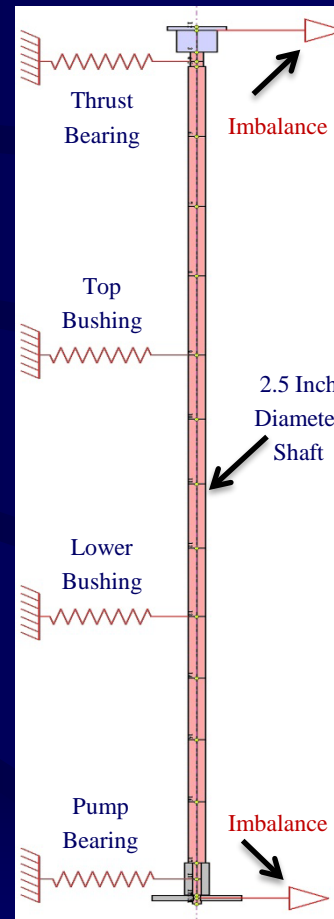
# Rotordynamics Analysis

- Gather Data from Disassembled Unit
- Dimensions and Weights of all Rotating Parts
- Evaluate Bushing Dimensions
- Determine Properties of Liquid Sulfur
- Translate into Finite Element Model
- Match Model to Observed Vibrations
- Design New Components to Fix Problem

# Actual System Compared to Model



## FEA Model



# Center Two Rotating Sleeves



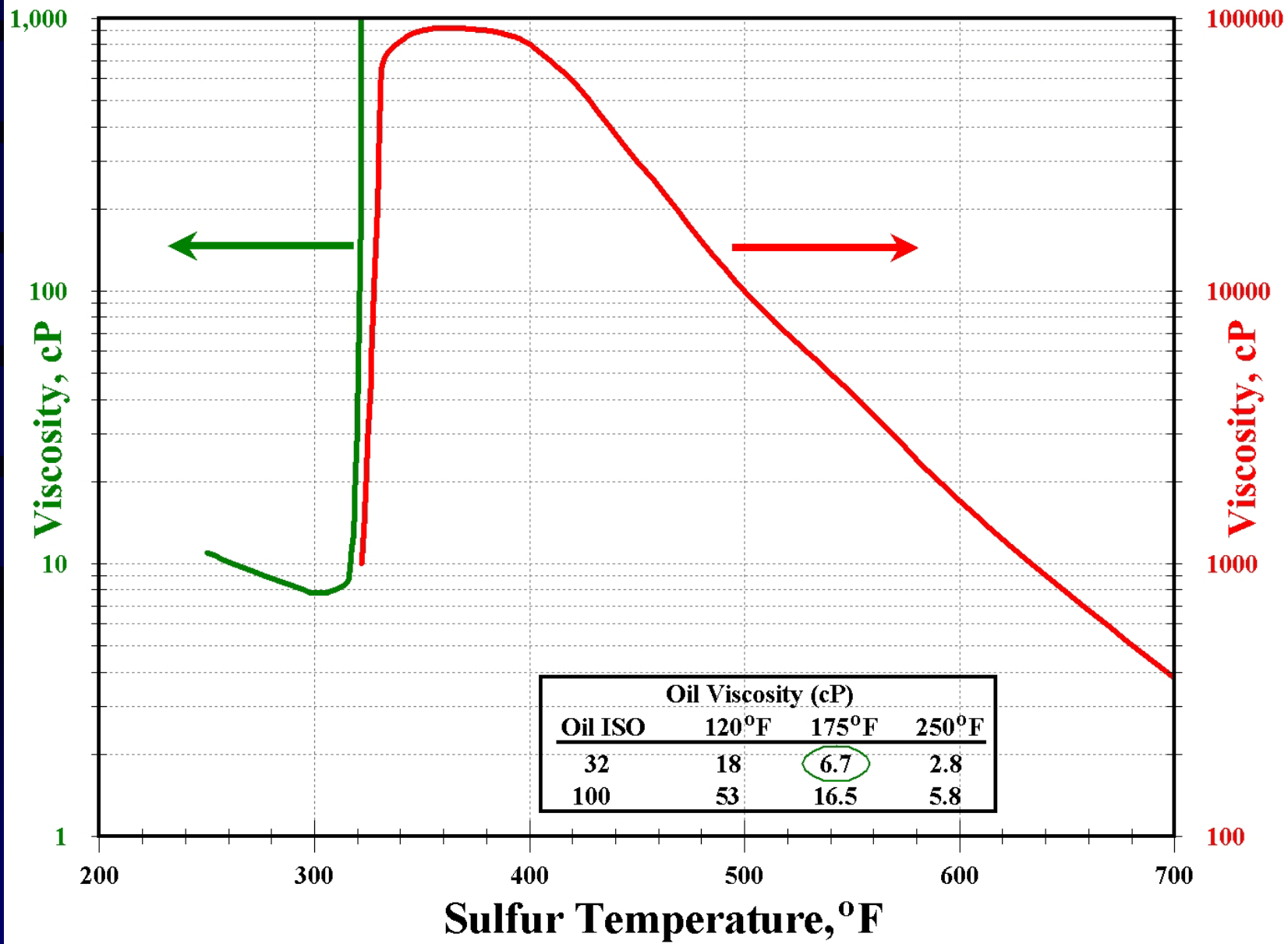
# Properties of Molten Sulfur

- Unusual Material
- Room Temperature Sulfur is a Crystalline Solid
- Fully Liquid at 235°F
- Forms Long-Chain Molecules – Gamma Sulfur
- Highly Non-Linear Viscosity
  - 7.8 cP at 300°F      **93,000 cP at 350°F**
- Sump Temperature Control Very Important

# Crystalline Solid Sulfur



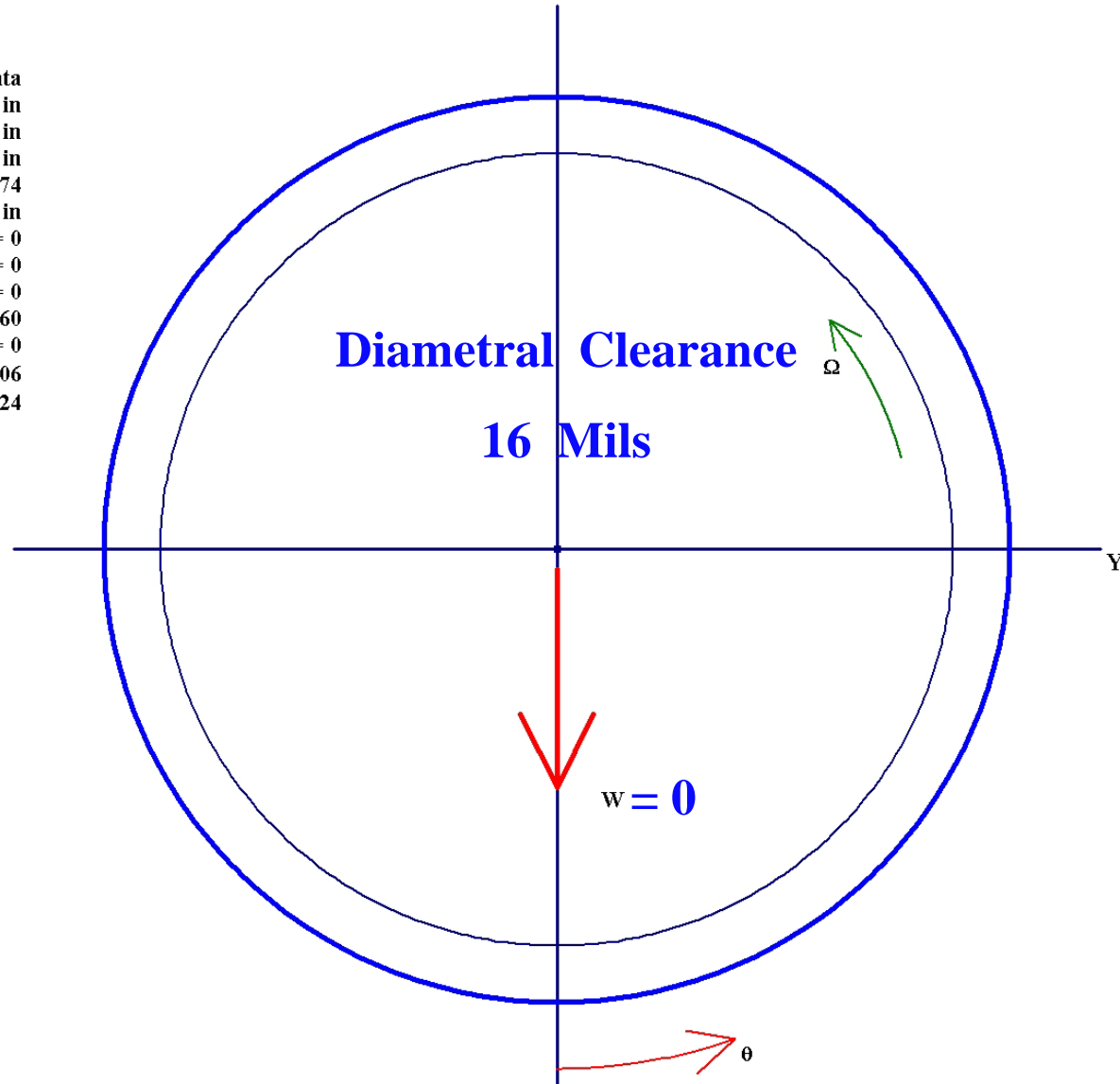
# Sulfur Viscosity v. Temperature



# Original Bushing Design

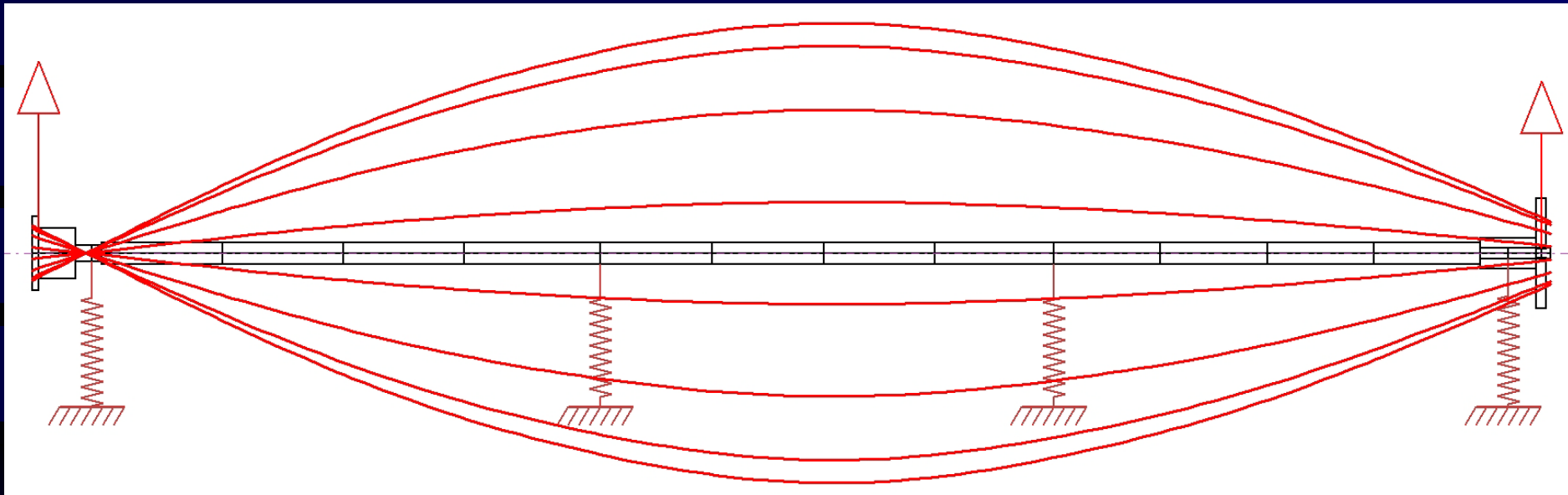
Original Sulfur Pump Bushing

Bearing Data  
L = 4.25 in  
Ds = 3.375 in  
Cb = 0.008 in  
2Cb/D = 0.00474  
Cp = 0.008 in  
Preload = 0  
Offset = 0  
Theta1 = 0  
Theta2 = 360  
Load Angle = 0  
Viscosity = 1.2E-06  
Density = 0.06424





# First Critical Speed Mode Shape



Calculated Frequency = 1,770 CPM  
With Original Upper and Lower Bushings

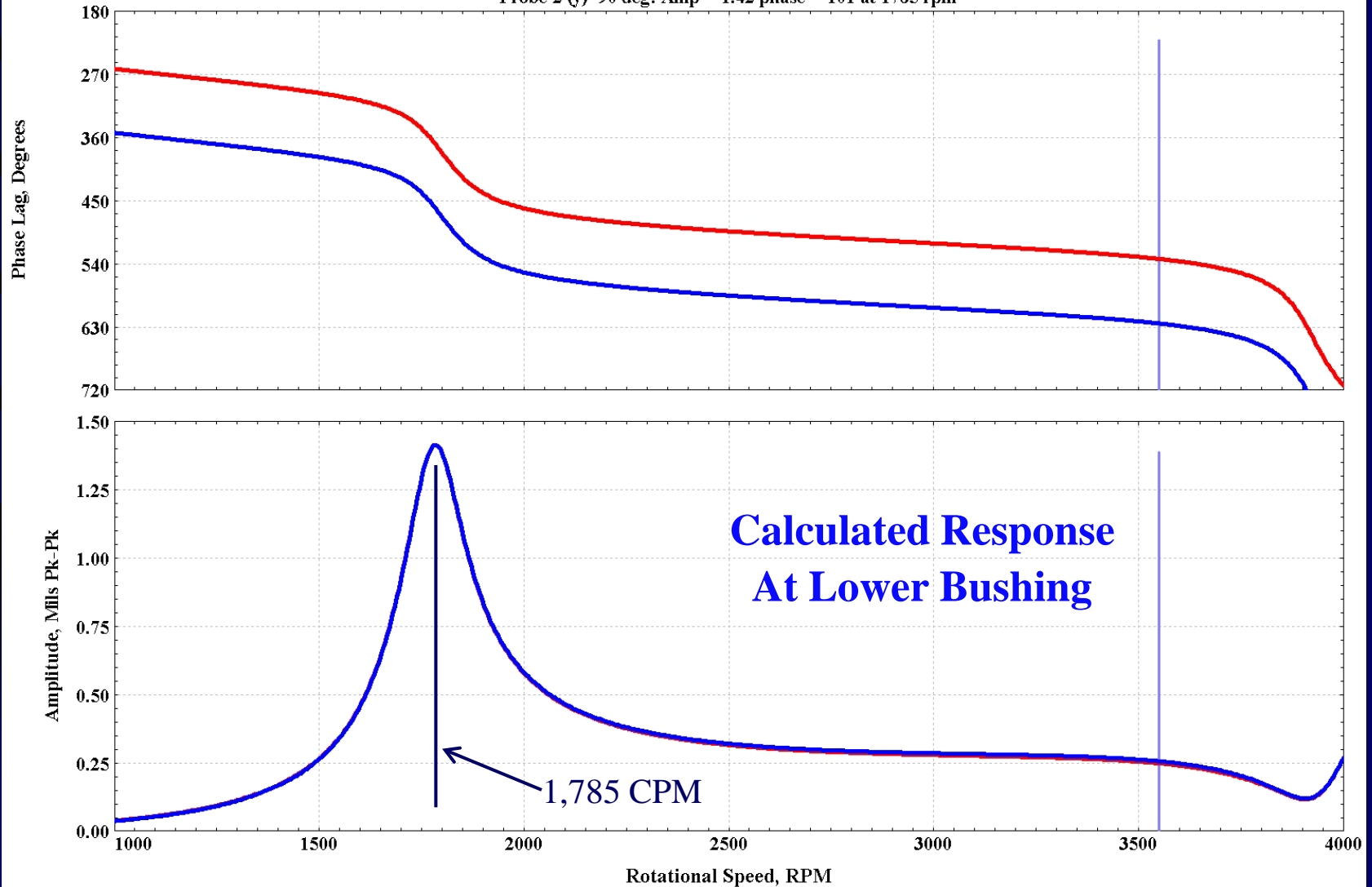
# Original Unbalance Response

Bode Plot - Pump Shaft Lower Middle Bushing

Station: 13, Sub-Station: 1

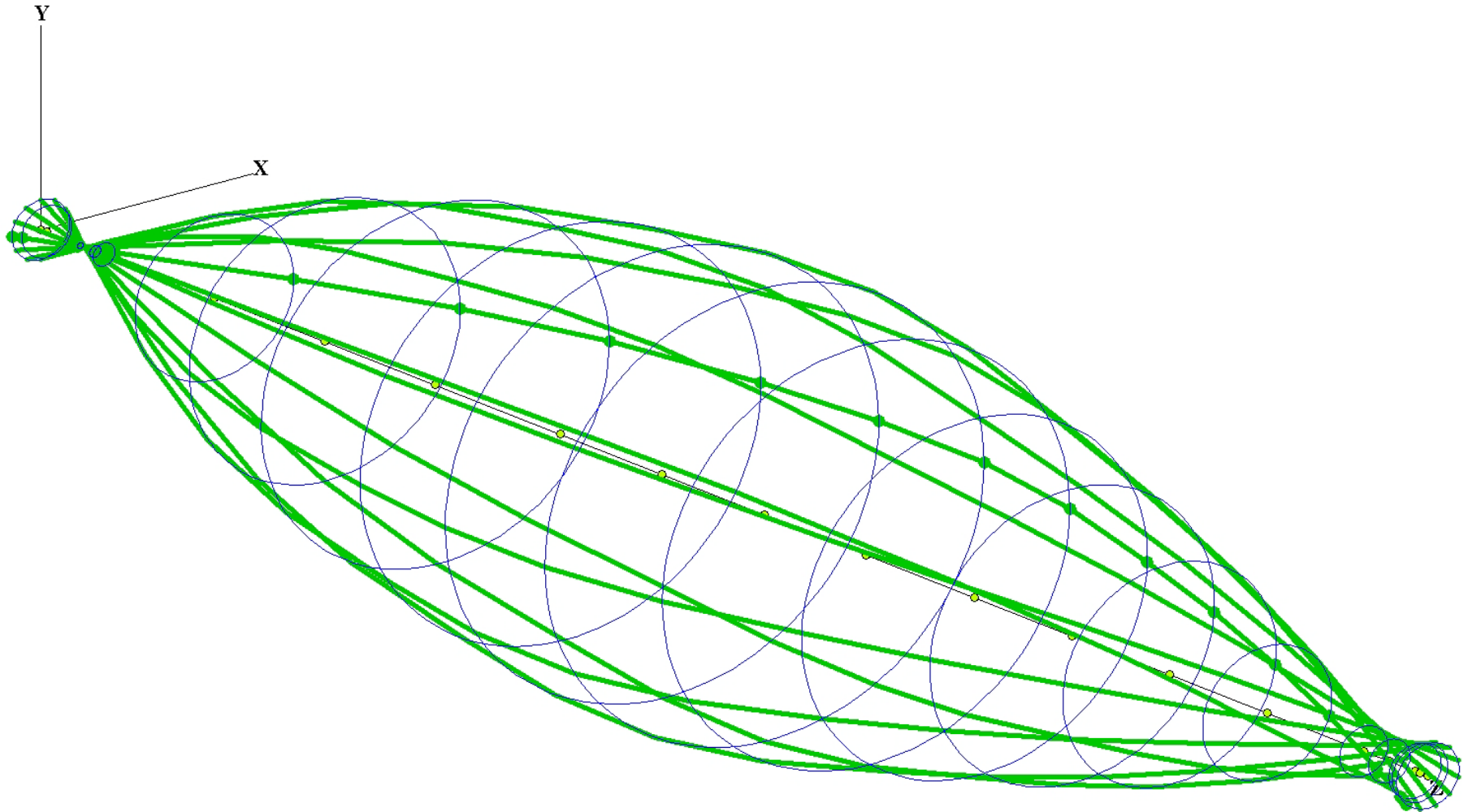
Probe 1 (x) 0 deg: Amp = 1.42 phase = 10 at 1785 rpm

Probe 2 (y) 90 deg: Amp = 1.42 phase = 101 at 1785 rpm



# Stability with Original Bushings

Precessional Mode Shape - UNSTABLE FORWARD Precession  
Shaft Rotational Speed = 3575 rpm, Mode No.= 3  
Whirl Speed (Damped Natural Freq.) = 1780 rpm, Log. Decrement = -0.3613



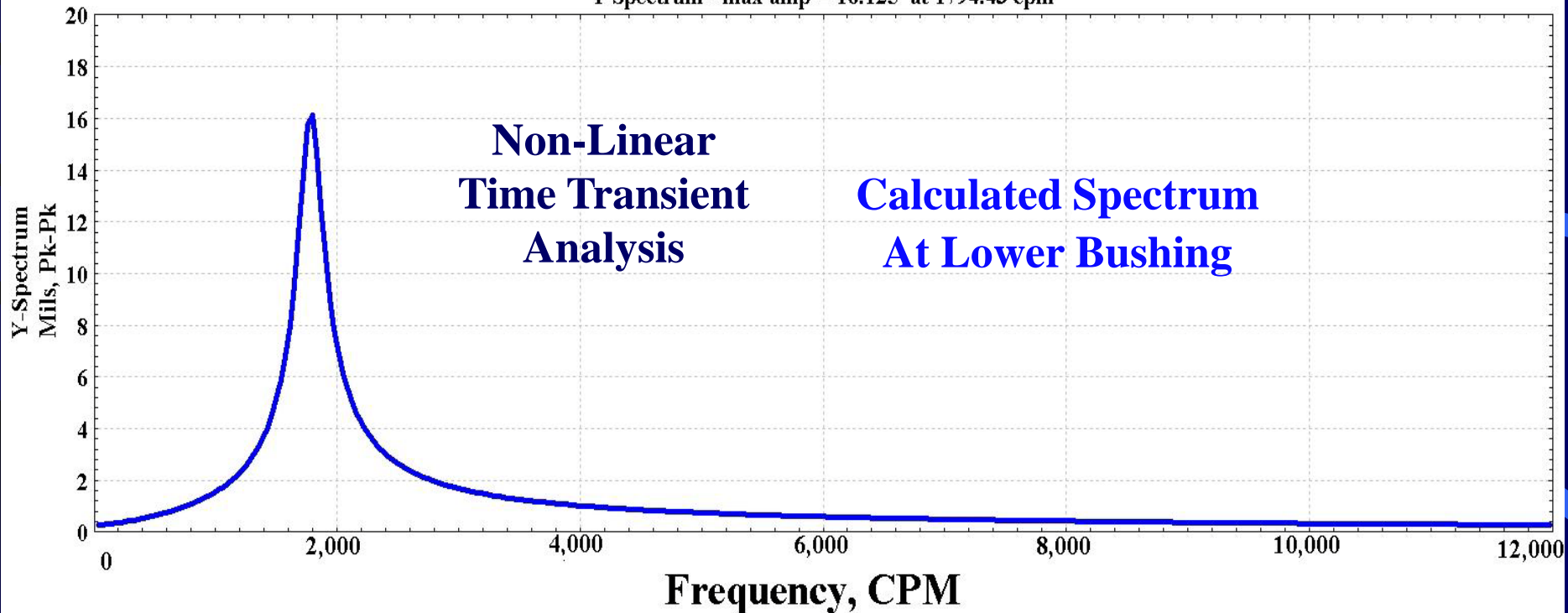
# Stability with Original Bushings

Original Bushings with 16 mils Diametral Clearance

Station: 13, Delta Freq.= 36.62 cpm

X Spectrum - max amp = 15.804 at 1794.43 cpm

Y Spectrum - max amp = 16.125 at 1794.43 cpm



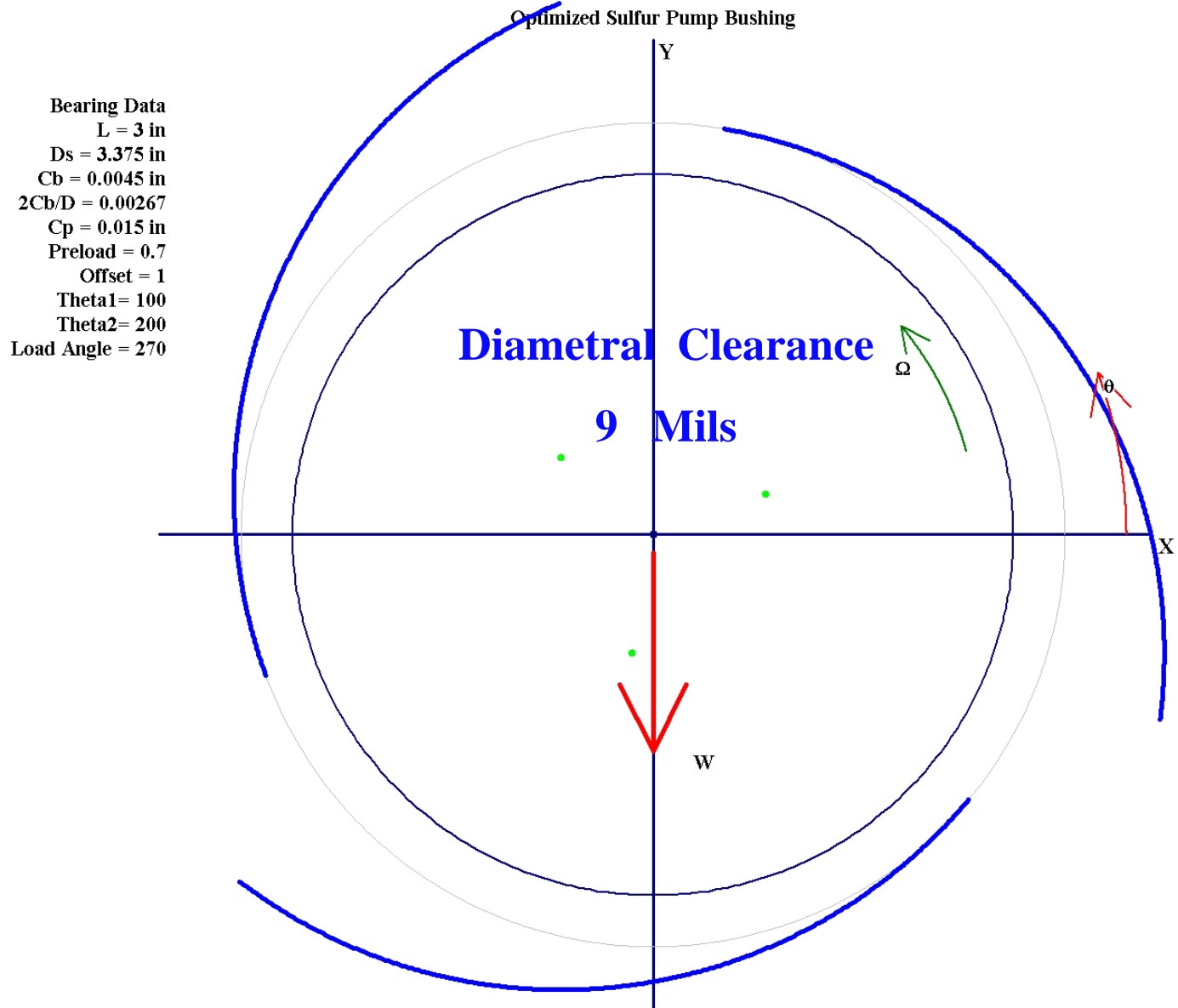
# Evaluation

- Shaft Critical Speed at  $\frac{1}{2}$  Operating Speed
  - Structural Resonance at  $\frac{1}{2}$  Operating Speed
  - Inherently Unstable Plain Circular Bushings
- 
- **Need To Control The Rotor Vibration**
  - **Center Two Bushings Logical Items to Revise**

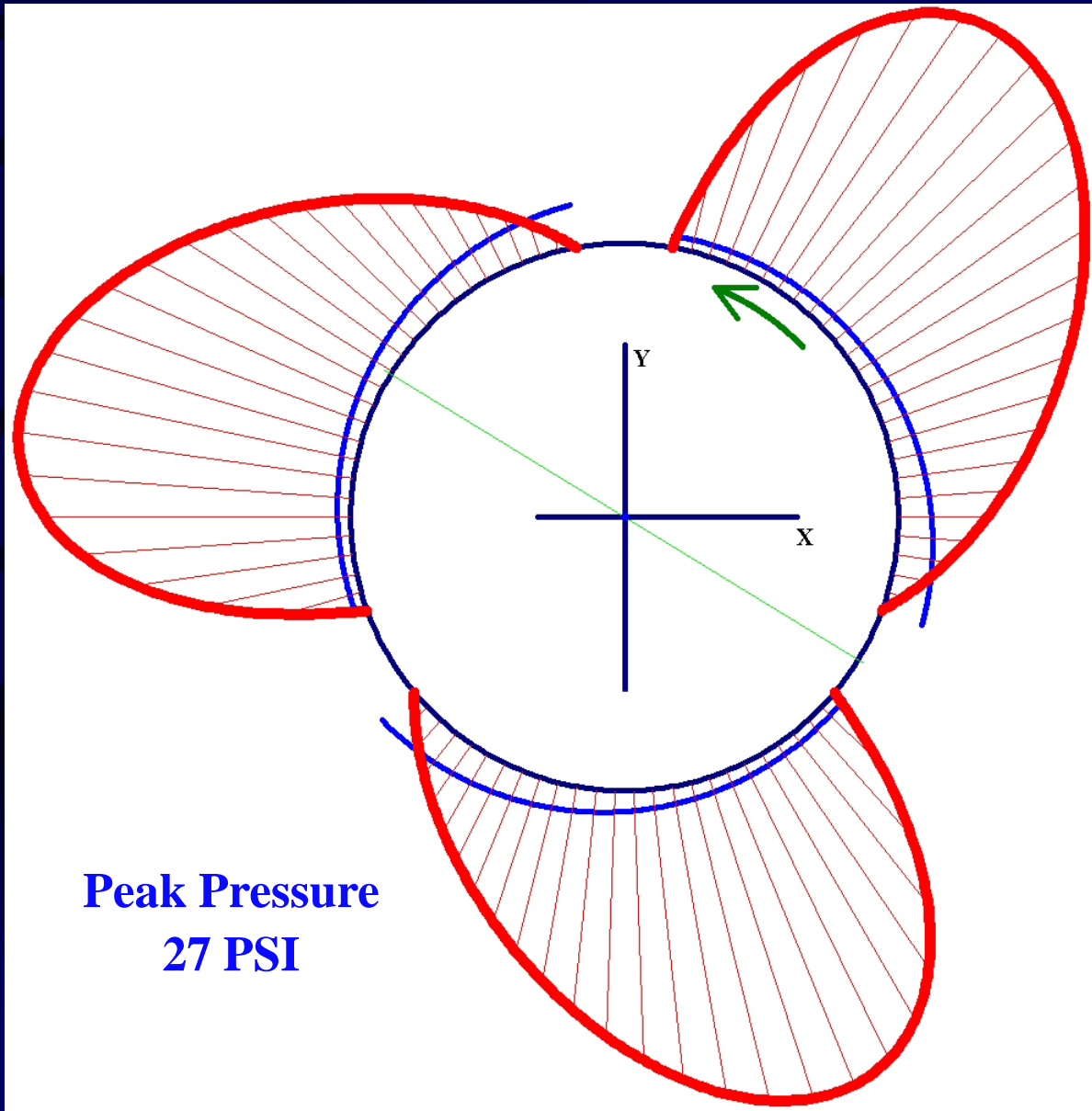
# Solution Goals

- Design New Upper and Lower Bushings
  - Increase Direct Stiffness
  - Raise Critical Speed above Operating Speed
  - Eliminate Instability
  - Assure Low Operating Speed Vibration
  - Increase Reliability and Reduce Costs

# Optimized Bushing Design



# Optimized Bushing Pressure Profile





# Bushing Stiffness and Damping Coefficient Comparison at 3,575 RPM

Bushing Type	Principal Stiffness, LB/IN	Principal Damping, LB-SEC/IN	Cross-Coupled Stiffness, LB/IN	Horsepower Loss
Plain Bushing	1,830	407	-69,400	0.65
3-Lobe Bushing	49,100 (26.8 Times Stiffer)	323	-20,700	0.38

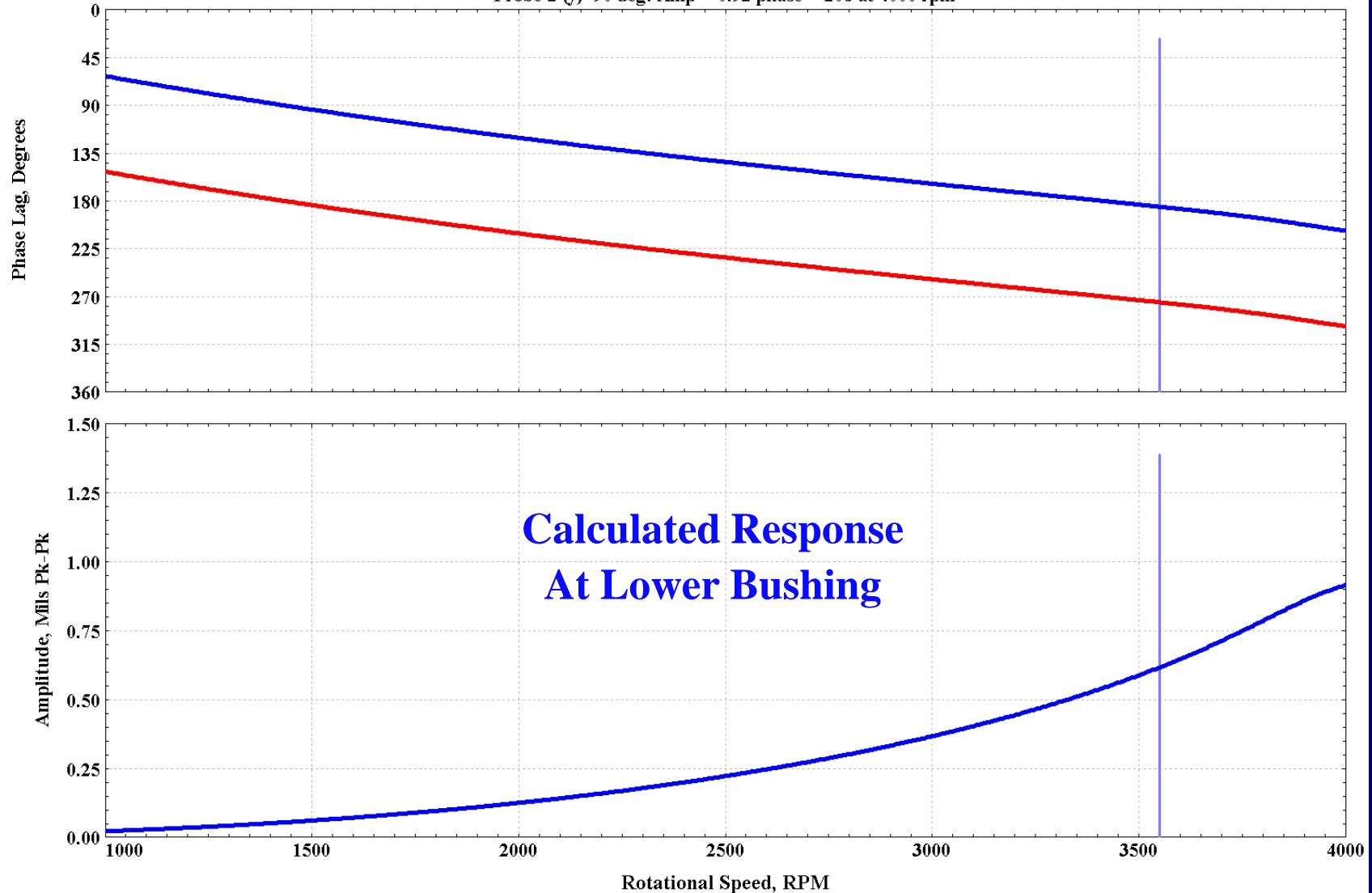
# New Design Unbalance Response

Bode Plot - Predicted Vibration at Lower Middle Bushing with 3-Lobe Bearings

Station: 13, Sub-Station: 1

Probe 1 (x) 0 deg: Amp = 0.92 phase = 118 at 4000 rpm

Probe 2 (y) 90 deg: Amp = 0.92 phase = 208 at 4000 rpm



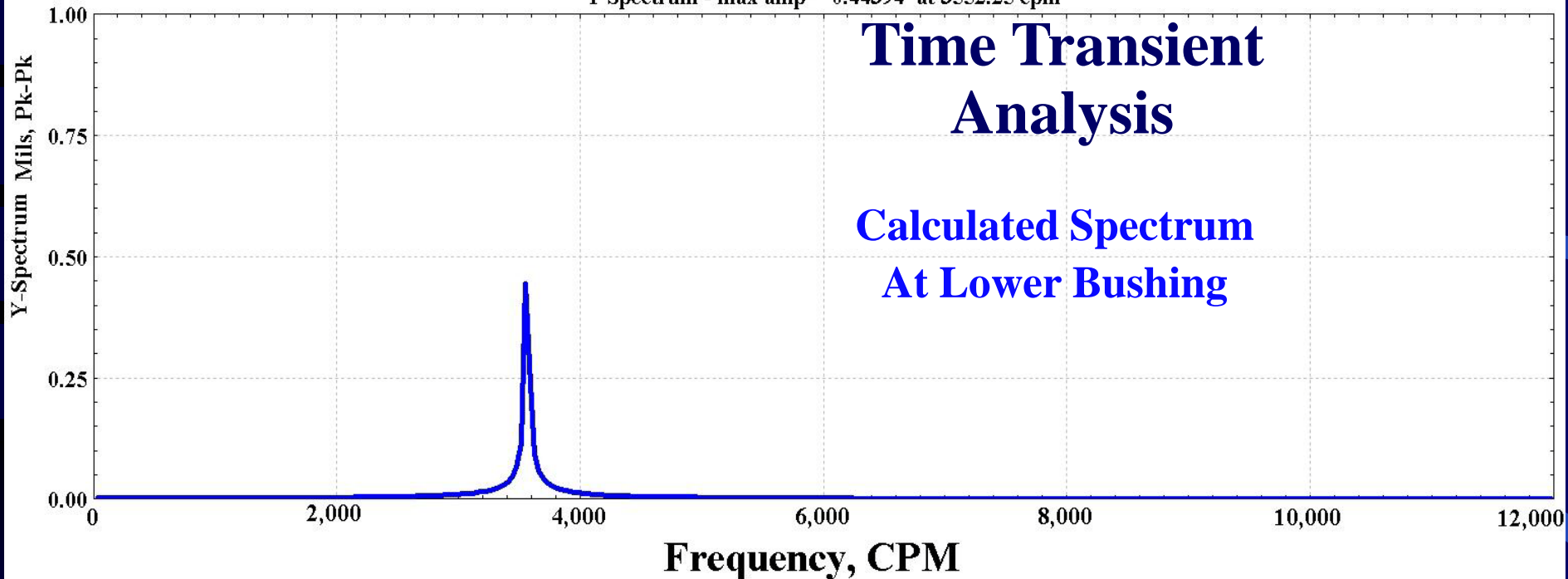
# Stability with New Design Bushings

Calculated Vibration at Lower Middle Bushing with 3-Lobe Design

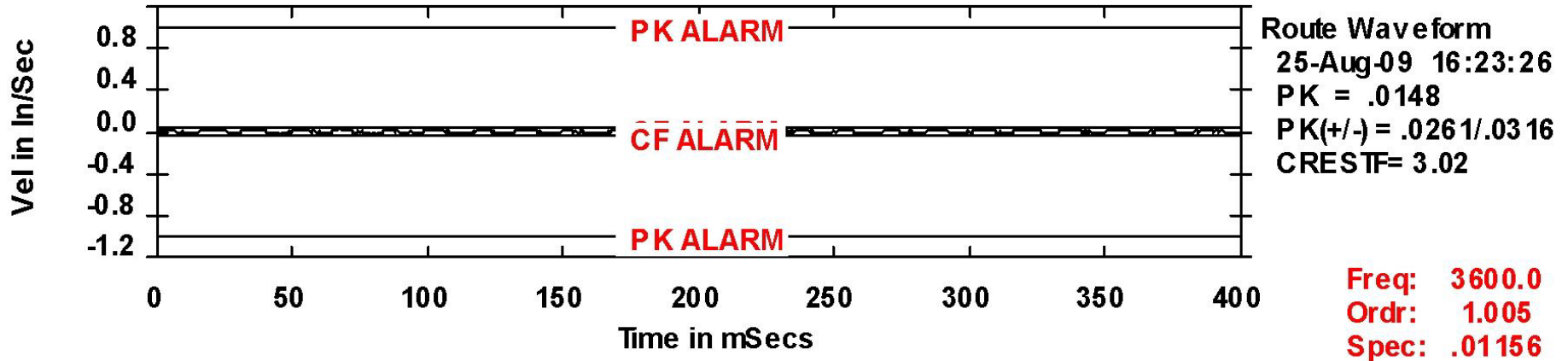
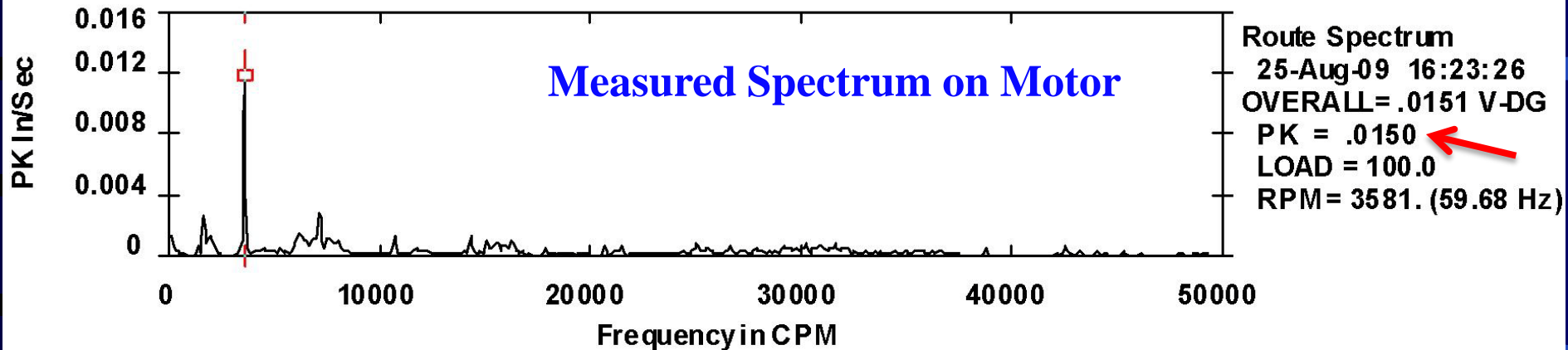
Station: 13, Delta Freq.= 36.62 cpm

X Spectrum - max amp = 0.44365 at 3552.25 cpm

Y Spectrum - max amp = 0.44394 at 3552.25 cpm



# Final Result



# Conclusion

- Vibration Problem Eliminated
  - Replaced 2 Plain Bushings with Profile Design
    - ✓ Inexpensive
    - ✓ Available Locally
  - Eliminated Critical Speed
  - No Structural Modifications Necessary
  - Reliability Increased and Costs Reduced