

CHALLENGES FOR PUMPS HANDLING HOT REFINERY RESIDUUM

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BACKGROUND

- Visbreaker Unit was commissioned in September 1997.
- Two (2) Pumps are in Feed service. Two (2) Pumps are in Fractionator Bottoms Service.
- All pumps are handling hot Crude Oil Residuum with Coke particles.

PROBLEM STATEMENT

- Initially MTBF was low, Year 2000 - 0.4 months.
- Seal failures were predominant (about 80%).
- 10% failures were bearing related.
- High production losses due to plant shutdowns.
- Two (2) fires on the Bottoms Pumps with extensive damage to the pumps.

PUMP DUTY

| | Feed | Fract. Botts. |
|-------------------------|------|---------------|
| Normal capacity (USGPM) | 1050 | 2042 |
| Differential Head (ft) | 1405 | 982 |
| Pump Speed (rpm) | 3550 | 3550 |
| Pumping temperature (F) | 520 | 662 |
| Viscosity at PT (cp) | 24.0 | 1.8 |

PUMP DUTY

| | Feed Service | Fract. Botts. Service |
|-------------|---|---|
| Seal Design | API 682 Type C – Tandem arrangement 2 | API 682 Type C – Tandem arrangement 2 |
| Seal Plans | Plans 32/52. | Plans 32/52. |
| Pump Size | 6x8x13.5 4x6x15 | 8x10x16 |
| Pump Design | API Code BB2 | API Code BB2 |

Steps To Solve The Problem

- Checked with Visbreaker Licenses and other Users. Feedback was similar to our experience.
- A significant effort including several Root Cause Analyses (RCA's) from 2000 to present was expended.

Steps To Solve The Problem – Low Cost Initiatives

- **First approach was to address low cost initiatives e.g. Improve seal design, Q.A. repair.**

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|--|
| <ul style="list-style-type: none">■ The Hastelloy Bellows subject to shearing and temperature set.■ Plan 52 buffer pot not vented <p>.</p> | <ul style="list-style-type: none">■ Hastelloy is not suited for high temp. Changed to Inconel 718 with drive lugs.■ See “other future action plans” |

Steps To Solve The Problem – Low Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|--|
| <ul style="list-style-type: none">■ Seal faces being scored and residuum solidifying in the outer seals.■ Cooling water inadequate due to header plugging. | <ul style="list-style-type: none">■ External Seal Oil Flush (Plan 32) was unreliable. A flow meter, valve and pressure gauge added.■ Buffer pot cooling water - project is underway to improve. |

Low Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|---|
| <ul style="list-style-type: none">■ Pressure builds in the buffer tank causing reverse pressurization and at times dislodging inner seal stationary seat. | <ul style="list-style-type: none">■ Plan 32 Flush unreliable. Instrumentation added.■ Better seat retainer required.■ Tangential ports used instead of radial ports. Buffer fluid changed to synthetic oil (5 to 8 cs @ 104 F). |

Low Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|--|
| <ul style="list-style-type: none">■ Different bearings running at different temperatures - some would exceed 250 F (Bearing housing skin) and run to failure. Others would stabilize at 230 F max.■ Shaft lockup caused by thermal growth. | <ul style="list-style-type: none">■ Slight variances in the bearings were deciding whether “go” or a “no-go”.■ Dual oil mist re-classifiers installed and jets directed at the bearing balls.■ Ensured adequate axial clrs (.072” min.) at radial bearing. |

Low Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|--|---|
| <ul style="list-style-type: none">■ Bearing to steel shaft(2.5 – 3”) fit for most pumps require an interference (.0000 - .0005” – k5 or k6 or j6).■ Bearing to housing fit for most pumps require a loose fit (.0000 - .0005”). | <ul style="list-style-type: none">■ For these particular pumps, bearing to alloy steel (416SS) shaft require a loose fit (.0000 - .0003” – j5).■ For these pumps, bearing to housing fit require a looser fit (.001 - .002” – j5). |

Low Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|---|
| <ul style="list-style-type: none"><li data-bbox="300 505 1073 715">■ The preceding general guidelines are wrong for these particular pumps.<li data-bbox="300 839 1073 1049">■ Bottoms Pumps experienced cavitation due to hole size on the suction strainer (1/8"). | <ul style="list-style-type: none"><li data-bbox="1111 505 1734 715">■ Detailed QA/QC sheet developed and used to support shop repair.<li data-bbox="1111 839 1778 968">■ Changed to screens with 5/8" holes. |

Steps To Solve The Problem – High Cost Initiatives

- Our second approach was to research the problem further, seek advice from consultants, then to engineer carefully the more expensive measures necessary

High Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|--|---|
| <ul style="list-style-type: none">■ Seal faces being scored and residuum solidifying in the outer seals. | <ul style="list-style-type: none">■ To improve the Plan 32, a Booster system for flushing installed. It consisted of dual pumps, dual filters, surge tank and instrumentation. Installed cost – US\$ 120,000. Completed mid 2003. |

High Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|--|
| <ul style="list-style-type: none">■ Pumps were oversized and Nss was high, about 13,000.■ Bottoms Pumps sometimes run at 32 – 46% of BEP whereas the minimum flow should be 50% of BEP. Flow could drop to as low as 5%. | <ul style="list-style-type: none">■ Need to buy pumps with a better hydraulic fit.■ Commissioned one new feed pump in 2004, cost – US\$ 200,000. For one new bottoms pump, order placed Sept. 2007. |

High Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|--|
| <ul style="list-style-type: none">■ Different bearings would run at different temperatures - some would surpass 250 F and run to failure.■ By design, sleeve bearings would be insensitive to thermal expansion effects. | <ul style="list-style-type: none">■ Bearing housing skin temperature < 180F are desired:<ul style="list-style-type: none">- - For new feed pump, fan cooled ball bearings used.- - For bottoms service, sleeve bearings are now specified. |

High Cost Initiatives

| OBSERVATIONS | CONCLUSIONS / ACTIONS |
|---|--|
| <ul style="list-style-type: none">■ For the feed pump (2 Stage), the inter-stage seal cavity was subject to high pressures (160 to 200 psig). This was causing overheating at the seal faces. | <ul style="list-style-type: none">■ For the new pump, the inter-stage end seal cavity was fitted with Colmonoy and Graphalloy throat bushings on either side of the leak-off to reduce the pressure to 120 to 150 psig . |

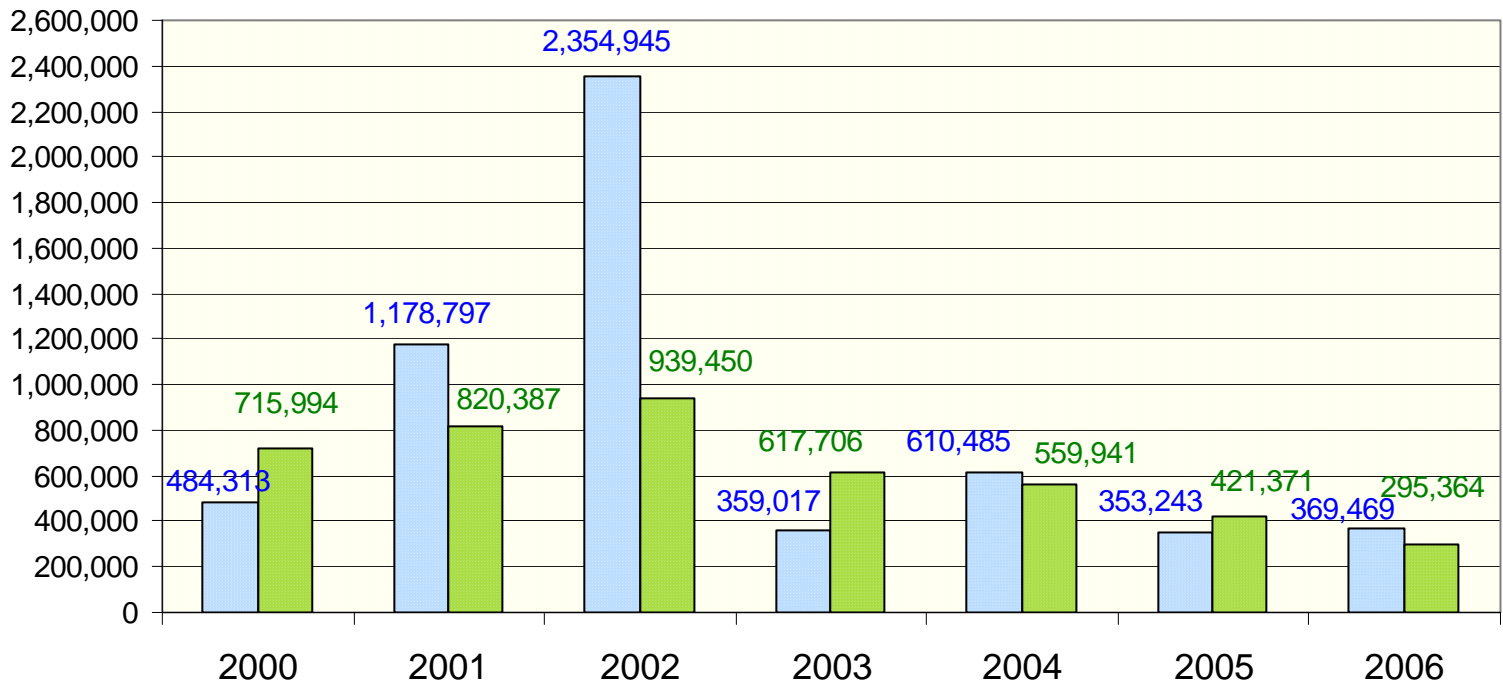
RESULTS REALIZED

- MTBF has been improved from 0.4 months (in Year 2000) to 12 months (in Year 2006).
- Occasional Bearing housing skin temp of 250 F on the old pumps have reduced to 230 F max.
- Maintenance cost per pump p.a. has reduced US \$ 158,000. in year 2001 to US \$ 53,000. in 2006.
- Production losses substantially reduced.

RESULTS REALIZED

**Average Maintenance Costs
per Pump p.a. (TT\$)**

- VBU Charge/Feed Pumps
- 4700/4701/4756
- Fractionator Bottoms Pumps
- 4707/4708



LESSONS LEARNED

- Even properly installed API-52 & 53 plans with barrier fluid pots are unsuitable for these services.
- If ball bearings are used, the design should limit bearing housing temp to 180 F max.
- Plan 32 flushes need to be properly designed with controls to maintain product isolation.
- Follow a specific repair procedure.

OTHER FUTURE ACTION PLANS

- To address the ultra-low bottoms flows (5% BEP) during plant startups and shutdowns :
 - ◆ Modify operating procedures.
 - ◆ Investigate control changes to enable more stable temperature and level control.
 - ◆ Install a minimum flow recycle loop.

OTHER FUTURE ACTION PLANS

- Install new dual mechanical seal arrangements (alternates) :
 - ◆ API 682 2CW-CS with steam as the buffer fluid.
 - ◆ API 682 3CW-BB (or FB) with plan 54 external barrier fluid circulator system.
- Upgrade the second pump in both services.

Picture 1: *East Pump Interstage End – Inner Seal
Face (Rotating)*



Picture 2: *West Feed Pump Interstage End – Inner Seal Face
(Stationary)*



*Picture 3: West Feed Pump Interstage End –
Inner Seal Bellows (Rotating)*



*Picture 4: West Feed Pump Suction End –
Inner Seal Face (Stationary)*

